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(54) ASSEMBLY FOR DEHYDRATING AIR TO BE SUPPLIED TO BLAST FURNACE

We, TAKASAGO THERMAL ENGI-NEERING COMPANY LIMITED and NIPPON STEEL CORPORATION, Japanese Body Corporates, respectively of 4—2, Kanda Surugadai, 5 Chiyoda-ku, Tokyo, Japan, and 6—3, Otema-chi 2-chome, Chiyoda-ku, Tokyo, Japan, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:-

The present invention relates to an assembly for dehydrating atmospheric air to be supplied to a blast furnace. It relates to such 15 an assembly wherein a combustion gas obtained by burning a waste gas containing inflammable components, such as a waste gas from a blast furnace, can be utilized for the regeneration of a regnerative moisture absorbent and wherein a relative humidity regulator, which does not need any external heat source, is provided for preventing the regenerative capacity of the moisture absorbent from being lowered.

In operation of a blast furnace variations in the moisture content of air supplied to the blast furnace cause the reactions in the furnace to undesirably fluctuate, and excessive moisture contents often adversely affect those reactions. Accordingly, it is desired that the moisture content of air supplied to a blast furnace be controlled so that it does not exceed a predetermined level irrespective of the seasons of the year.

Dehydration of air in the operation of a blast furnace involves various problems which are not encountered in other fields. Among others, when a blast furnace is operating, an extremely large quantity of air,

for example, as large as 5,000 to 12,000 40 Nm³/min (where N represents normal temperature and pressure) of air, is required. Atmospheric air may be compressed by a blower specially designed for supplying a large quantity of air to a blast furnace, to form a stream of air having a temperature of 150 to 250°C and a pressure of 3.5 to 5.0 Kg/cm² gauge. The stream of air so formed is further heated in hot air furnaces to a temperature of 500 to 1200°C before it is introduced into a blast furnace. Obviously, dehydration of atmospheric air at the input side of the blower would be technically less difficult than dehydration of compressed air at the discharge side of the blower.

However, when a large quantity of atmospheric air is dehydrated using a regenerative moisture absorbent, a large quantity of hot air is required for the regeneration purpose, and, thus, it is necessary to provide a powerful external heat source. Some existing plants utilize electric energy, hot gases or steam as the external heat source. Obviously, this is not advantageous from the point of view of heat economy.

It would appear that air could be advantageously cooled and partially dehydrated by means of a cooler, before the air is subjected to the action of a regenerative moisture absor-bent. However, if the air, which has passed the cooler and has had its temperature lowered and relative humidity increased, is brought into contact with the regenerative hygroscopic moisture absorbent, there is the possibility of the problem of the deliquescence of the moisture absorbent arising. While typical moisture absorbents, such as lithium chloride, are highly hygroscopic, they often undergo



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deliquescence when they have absorbed an excessive amount of moisture. The service life of a rotor having such a moisture absorbent therein will be shortened, if it is caused to operate under such conditions that deliquescence of the absorbent would occur.

Moreover, atmospheric air available in an iron foundry normally contains a quantity of impurities. When a large quantity of such air 10 is treated by a rotor containing a moisture absorbent, those impurities are caught by and accumulated in the absorbent and adversely affect the absorbent.

In accordance with the invention there is provided a dehydration assembly for dehydrating atmospheric air to be supplied to a blast furnace, comprising:

a casing, the inside space of which is divided into regenerating and dehydrating

zones by a partition plate;

at least one gas permeable rotor containing a regenerative moisture absorbent and rotatably mounted in said casing so as to radially extend across cross-sections of said regenerating and dehydrating zones;

a pre-cooler located in said dehydrating zone upstream of said rotor or rotors with respect to the flow of air to be dehydrated in

the dehydrating zone in use;

an after cooler located in said dehydrating zone downstream of said rotor or rotors;

a relative humidity regulator located in said dehydrating zone between said pre-cooler and said rotor or rotors;

piping means for circulating heat transfer medium through said relative humidity regulator and through said after-cooler so as to effect heat transfer between the two;

an outlet from the dehydrating zone for dehydrated air leaving said after-cooler; and an inlet for introducing a hot gas into said

regenerating zone.

In a preferred form the invention provides a dehydration assembly for dehydrating atmospheric air to be supplied to a blast furnace, comprising:

a casing, the inside space of which is divided into regenerating and dehydrating

zones by a partition plate;

at least one gas permeable rotor containing a regenerative moisture absorbent and rotatably mounted in said casing so as to radially extend across cross-sections of said regenerating and dehydrating zones;

a pre-cooler located in said dehydrating zone upstream of said rotor or rotors with respect to the flow of air to be dehydrated in

the dehydrating zone in use;

a first after-cooler located in said dehydrat-60 ing zone downstream of said rotor or rotors;

a second after-cooler located in said dehydrating zone downstream of said first aftercooler:

a relative humidity regulator located in said dehydrating zone between said pre-cooler

and said rotor or rotors;

piping means for circulating heat transfer medium through said relative humidity regulator and through said second after-cooler so as to effect heat transfer between the two;

an outlet from the dehydrating zone for the dehydrated air leaving said second aftercooler; and

an inlet for introducing a hot gas into said

regenerating zone.

The invention also includes a blast furnace installation wherein dehydrated air is supplied to the furnace by a blower, and an air dehydration assembly as described above is arranged with its outlet from the dehydrating zone connected to the input side of the blower, and its inlet to the regenerating zone connected with a source of combustion gas obtained by burning a waste gas containing inflammable components.

Preferably the or each said gas permeable rotor comprises a layer containing the regenerative moisture absorbent and a layer containing an adsorbent capable of adsorbing gaseous impurities contained in the air to be dehydrated, said layer containing the impurity adsorbent being superimposed on said layer containing the moisture absorbent and located upstream of said layer containing the moisture absorbent with respect to the stream of air in the dehydrating zone in use, whereby the air to be dehydrated passes through said layer containing the impurity adsorbent before it passes through said layer containing the moisture absorbent.

Preferably a clearance formed between each of two opposed flat surfaces of the or each said rotor and an edge of the partition plate facing said flat surface of the rotor is sealed by a packing element securely fixed on 105 said edge and having two spaced parallel arms extending lengthwise of said edge and contacting the rotor to form a substantially sealed space and, for that space formed upstream of the rotor with respect to the stream of hot gas 110 passing through the regenerating zone in use, there is provided means for communicating said space with a region downstream of said rotor in the regenerating zone.

The invention will be further described 115 with reference to the accompanying drawings which illustrate embodiments of the invention and their use and in which:

Figure 1 illustrates diagrammatically the incorporation of one embodiment of the 120 invention in a blast furnace installation;

Figure 2 is an enlarged vertical sectional view of the dehydration assembly shown in Figure 1:

Figure 3 is a diagrammatic view illustrating 125 one form of circulation passages of a heat transfer medium for the various devices arranged in the dehydrating zone in the dehydration assembly of Figure 2;

Figure 4 is a diagrammatic view illustrating 130

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another form of circulation passages of a heat transfer medium for the various devices arranged in the dehydrating zone of a modified form of dehydration assembly;

Figure 5 is an enlarged cross-sectional view of the dehydration assembly of Figure 2, taken along the line V—V, as seen from the direction indicated by the arrows V;

Figure 6 is a perspective view showing one of the rotors of the dehydration assembly shown in Figure 2;

Figure 7 is a cross-sectional view of the dehydration assembly of Figure 2, taken along the line VII—VII, as seen from the

direction indicated by the arrows VII; Figure 8 is a partially cut away perspective view for illustrating a sealing means between a rotor and the partition plate, and:

Figure 9 is an enlarged cross-sectional view for illustrating the sealing means between the rotor and the partition plate.

In the various figures the same reference numerals have been used for equivalent parts.

Referring to Figure 1, the illustrated installation for supplying air to a blast furnace 10 comprises, in addition to hot air furnaces 11 and a blower or compressor 12 specially designed for use in the operation of a blast furnace, a dehydration assembly 13 for dehydrating air to be taken up by the blower 12, and an arrangement of the installation for converting a hot waste gas, such as a waste gas from the blast furnace, to a hot gas required for the regeneration of a regenerative hygro-35 scopic material used in the dehydration assembly 13, the latter arrangement comprising a cooling dehydrater 4, a gas cleaner 5 and a combustion device 6.

The blower 12 is of such a size that it can provide 5,000 to 12,000 Nm³/min of air, depending on the size of the blast furnace 10, the air having a temperature of 150 to 250°C and a pressure of 3.5 to 5.0 Kg/cm² gauge, at

the output side of the blower.

The dehydration assembly 13, which will be described hereinafter in detail, comprises a casing 14 having arranged therein a rotor 15 containing a regenerative hygroscopic substance, a pre-cooler 16, an after-cooler 17 and

50 a relative humidity regulater 18.

The cooling dehydrater 4 comprises a casing having arranged therein a cooler 19, through which cold water from a refrigerator (not shown) is circulated, a coarse filter 20 and a mist separator 21. A moist gas obtained by passing a waste gas from the blast furnace 10 through a conventional scrubber (not shown) is cooled and dehydrated by the cooling dehydrater 4. The gas introduced into the 60 cooling dehydrater 4 contains a quantity of combustible substances and impurities. For example, it may contain 19.2% by volume of CO_2 , 24.7% by volume of CO, 5.3% by volume of H_2 , 50.3% by volume of N_2 , 0.001 g/Nm³ 65 of Na, 0.001 g/Nm³ of K and a trace of S.

When such a moist gas containing impurities is passed through the cooling dehydrater 4, the moisture in the gas is condensed and most of the impurities, including sodium hydroxide, potassium hydroxide and other impurities, are removed together with the condensed water by way of a drain 22.

The gas cleaner 5 comprises a casing having operatively arranged therein a filter 23 comprising a layer of an adsorbent such as activated carbon and a high performance filter 24, for example, a HEPA filter. Any impurities which have survived the abovementioned cooling and dehydration treatment will be removed by the gas cleaner 5.

The combustion device 6 is a gas burner equipped with a propane gas pilot burner. The cleaned gas coming from the gas cleaner 5 through a conduit 26 is burnt in the combustion device 6 with the aid of air supplied through a conduit 27. The combustion gas obtained in the combustion device 6 is a hot gas essentially composed of CO, and N, with few impurities. This hot gas is used for the regeneration of the hygroscopic substance 90 in the rotor 15.

The details of the dehydration assembly 13 in accordance with the invention will now be described with reference to Figures 2 through

Referring to Figures 2 and 7, the illustrated dehydration assembly 13 comprises a generally rectangular steel casing 14, the inside space of which is divided into two spaces 29 and 30 by a partition plate 28, said spaces 29 100 and 30 constituting regenerating and dehydrating zones; two gas permeable rotors 15, 151 containing a regenerative moisture absorbent rotatably mounted in said casing 14 so as to radially extend across the cross-sections of 105 the regenerating and dehydrating zones 29 and 30; a pre-cooler 16 located in the dehydrating zone 30 upstream of said rotors; an after-cooler 17 located in the dehydrating zone 30 downstream of said rotors; a relative 110 humidity regulator 18 located in the dehydrating zone 30 between said pre-cooler 16 and said rotors; piping means for circulating the same heat transfer medium through said relative humidity regulator 18 and an after-cooler 31 located downstream of said aftercooler 17 (the piping means is not shown in Figure 2, but the details thereof are shown in Figure 3); a conduit 32 for passing the dehydrated air leaving said after-cooler 17 and after-cooler 31 to the blower 12, and; a conduit 33 for introducing the hot gas obtained in the combustion device 6 into the regenerating zone 29

When the dehydration assembly is operat- 125 ing, the hot combustion gas is introduced into the regenerating zone 29 by means of a blower 34, which is mounted on the top of the casing 14 and is driven by a motor 35. The hot gas is then caused to pass through the rotor and 130

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discharged from the output side of the blower 34 through an outlet 36. Upon passing through the rotors the hot gas regenerates the hygroscopic substance in the rotors by taking away moisture from the hygroscopic substance. In the dehydrating zone 30, atmospheric air is introduced into the assembly 13 through an inlet 37 by means of the blower 12, cooled and partially dehydrated by passing through the pre-cooler 16, and has its relative humidity regulated by passing through the relative humidity regulator 18. The air is then permitted to pass through the rotors. Moisture of the air is absorbed by the hygroscopic 15 substance impregnated in the rotors, whereby the air is dried. Thereafter, the air has its sensible heat taken away by passing through the after-cooler 17 and the after-cooler 31 and is then passed through the conduit 32 to the 20 blower 12.

One of the important features of this assembly is the provision of the relative humidity regulator 18 and the piping means for circulating the same heat transfer medium through the regulator 18 and the after-cooler 31, in order to regulate the relative humidity of the air to be passed through the rotors in the dehydrating zone 30, thereby to avoid undesirable deliquescence of the moisture absorbent. Another feature of this dehydration assembly is in the structure of the rotors which is specially designed so that undesirable contamination of the moisture absorbent with impurites contained in the air may be avoid-35 ed. Still another feature of this dehydration assembly resides in the provision of sealing means which prevents the hot regenerating gas from leaking through clearances between the rotors and the partition plate 28 or through clearances surrounding the peripheral surface of the rotors. These and other features and advantages will be described in detail hereinafter.

Figure 3 is a diagrammatic view illustrating circulation passages of a heat transfer medium for the pre-cooler 16, the relative humidity regulator 18, after-cooler 17 and after-cooler 31. These devices may have substantially the same structure. Typically, each device may be a finned tube heat exchanger as shown in Figure 5. Water is circulated as a heat transfer medium through tubes of each of these heat exchangers. There is provided an independent water circulation passage 38 through which water is circulated by means of a pump 39 between the relative humidity regulator 18 and the after-cooler 31. Through the precooler 16 cold water cooled by a refrigerator 40 is circulated by means of a pump 41, whereas through the after-cooler 17 cold water from a cooling tower 42 is circulated by a pump 43. Cooling water for the refrigerator 40 is supplied from the cooling tower 42 by means of a pump 44. The function of the 65 relative humidity regulator 18 is to transfer

sensible heat of the dehydrated air leaving the after-cooler 17 to the air which has passed through the pre-cooler 16 and is about to enter the rotors, whereby reduction in the relative humidity of the air, which has passed through 70 the pre-cooler 16, can be achieved without the need of any external heat source. In one working example, in which atmospheric air at a temperature of 35°C was introduced into the dehydrating zone 30 of the dehydration 75 assembly of the invention, the air had a temperature of 15°C and a relative humidity of 95% when it left the pre-cooler 16. When it left the relative humidity regulator 18 it had a temperature of 20°C and a relative humidity of 70%. By passing the air through the rotors, most of the moisture content of the air was removed and the temperature of the air reached 47°C. The air was then cooled to a temperature of 40°C by the after-cooler 17 and to 35°C by the after-cooler 31. Thus, the relative humidity of the air, which enters the rotors, can be reduced to such a level that the hygroscopic substance, such as lithium chloride, impregnated in the rotors will not 90 undergo deliquescence.

Figure 4 illustrates a piping system for an embodiment of the invention which is simpler than that shown in Figure 3 and in which the heat transfer-medium, namely water, which has passed through the after-cooler 17, is passed to and circulated through the relative humidity regulator 18. More specifically, cold water from the cooling tower 42 is introduced into the after-cooler 17, where it is somewhat 100 warmed, and then passed through the piping 38 to the relative humidity regulator 18. The system shown in Figure 4 is advantageous in that the after-cooler 31 is not necessary and the load of the cooling tower 42 may be 105 reduced. Furthermore, the temperature of the water, which is circulated through the relative humidity regulator 18, may be somewhat higher than that in the case of Figure 3, and thus, the relative humidity of the air passing 110 through the regulator 18 may be reduced to a greater extent. The operation of the precooler 16 is the same as in Figure 3.

Figure 6 illustrates a specific form of the rotor which may be used in the dehydration 115 assembly of the invention. The illustrated rotor comprises a layer 44 containing a regenerative moisture absorbent and allayer 45 containing an adsorbent capable of adsorbing gaseous impurities contained in the 120 air to be debyrated, said layer 45 being located upstream of said layer 44 with respect to the stream of air in the dehydrating zone 30. The layer 44 comprises a gas permeable disc having a honeycomb structure made of 125 asbestos material impregnated with a regenerative moisture absorbent such as lithium chloride. The layer 45 comprises a gas permeable disc having a honeycomb structure made of asbestos material charged with a 130

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particulate adsorbent such as activated carbon or zeolite. Both layers 44 and 45 are preferably bonded together to form a unitary

When the rotor is operating, sulfur oxides and other gaseous impurities contained in the moist air passing through the layer 45 are adsorbed by the adsorbent, and in the regenerating zone 29 the adsorbed impurities are released from the adsorbent by the hot gas and discharged together with the waste hot gas. Thus, the adsorbent is regenerated, and this cycle of adsorption and regeneration is repeated. Since the moist air is caused to pass through the layer 45 containing the adsorbent before it passes through the layer 44 containing the moisture absorbent, the impurities are prevented from being caught by the moisture absorbent, such as lithium chloride, and from adversely affecting the absorbent. The moisture in the air is absorbed by the absorbent at the time the moist air passes through the layer 44 containing the absorbent, and the absorbed moisture is released by the hot gas in the regenerating zone 29 and discharged together with the waste hot gas. Thus, the moisture absorbent is regenerated.

Figure 7 is a cross-sectional view of the dehydration assembly of Figure 2, taken along the line VII-VII, as seen from the direction indicated by arrows VII, and illustrates a manner of mounting the rotors. As seen from Figure 7, two similar rotors 15 and 151 are mounted side by side. The rotors 15 and 15' are independently caused to rotate by driving endless belts 46 and 46' extending over the peripheral surfaces of the rotors by means of motors 47 and 471, respectively. Clearances between each rotor and the rectangular casing 14 are shielded by blind plates 48 and 481 in a manner as shown in Figures 6 and 7. The endless belt 47 or 471 extending over the peripheral surface of each rotor is positioned between the blind plates 48 and 48. The reference numerals 49 and 49. designate bearings securely supported by the partition plate 28, and the reference numerals 50 and 50^{T} designate shafts of the rotors 15 and 15, respectively. The hot regenerating gas is caused by the blowers 34 and 341 to flow through the regenerating zone 29 in a direction perpendicular to the sheet of paper, on which Figure 7 is drawn, from the face to the back, whereas the air to be dehydrated is caused by the blower 12 to flow through the dehydrating zone 30 in the opposite direction, that is in a direction perpendicular to the sheet of paper on which Figure 7 is drawn from the back to the face.

When the dehydration assembly is operating a part of the hot regenerating gas, which has reached each rotor tends to leak through a clearance formed between an end of the partition plate 28 and a flat surface of the 65 rotor facing said end into the stream of the

dehydrated air, which has passed through the rotor in the dehydrating zone 30. This is because the blower 12 is much more powerful than the blower 34 or 34' and also because the pressure of the dehydrated air which has passed through the rotor is lower than that of the hot regeneration gas which has just reached the rotor in the regenerating zone 29. Such leakage of the hot combustion gas contaminates the dehydrated air and causes various problems.

In a preferred embodiment therefore, there is provided means for preventing the regenerating hot combustion gas from leaking into the stream of the dehydrated air. Figure 8 is an enlarged partially cut away perspective view illustrating an edge of the partition plate 28 which is designated by the reference numeral 51 in Figure 2. On this edge of the partition plate 28 facing one of the flat surfaces of each rotor there is securely fixed a packing element having outwardly projecting spaced parallel arms 52 and 53 extending lengthwise of the edge of the partition plate 28. The packing element is so arranged that free edges of its arms 52 and 53 contact one of the flat surfaces of each rotating rotor and that the outermost ends 54 and 55 of each arm are in abutting engagement with an edge of an opening 56 provided in the blind plate 48 (Figures 7 and 9). Thus, there is formed a substantially sealed spaced 57 between the arms 52 and 53 of the packing element. A similar sealed space is also formed between the opposite flat surface of the rotor and the 100 end of the partition plate facing said flat surface. But only the sealed space 57 formed at that position designated by the reference numeral 51 in Figure 2 is communicated with a region downstream of the rotors in the 105 regenerating zone 29 by means of a communicating tube 58. Now referring to Figures 6 and 9, the communicating tube 58 is so arranged that it extends from the sealed space 57, passes through the blind plate 48 (as designated by 110 the reference numeral 59 in Figure 9), then through a space 60 between both blind plates 48 and 481 and then through the blind plate 481, and finally opens to a region downstream of the rotors in the regenerating zone 29. By 115 this means the regenerating hot combustion gas may be substantially prevented from leaking into the stream of the dehydrated air. Since the region downstream of the rotors in the regenerating zone has a lower pressure 120 than that of the region upstream of the rotor in the regenerating zone, any traces of the hot gas which have gone from the latter region beyond the arm 53 of the packing element into the space 57 are sucked through the 125 communicating tube 58 into the former region without being allowed to go beyond the arm 52.

In a modification, the diameter of the rotors

15, 15' may be somewhat smaller than that of 130

the opening 56, and the plates 48, 481 extend some distance over the peripheral edge of their respective rotors, so that a clearance is formed between the peripheral surface of each rotor and the corresponding opening 56 provided in the blind plates 48 and 481, this clearance being sealed by an annular packing element securely fixed on the circumferential edge of the opening 56 to prevent gas leakage

10 through said clearance.

The foregoing construction provides a dehydration assembly for dehydrating air to be supplied to a blast furnace wherein a waste gas available in an iron foundry may be utilised as a heat source for regenerating the used regenerative moisture absorbent. Furthermore, the cooled moist air may be dehydrated without the problem of the deliquescence of the regenerative moisture absorbent arising. Also, atmospheric air containing a quantity of impurities, such as available in an iron foundry, may be dehydrated without suffering from reduction in the regenerative capacity of the absorbent due to contamina-25 tion by those impurites. In addition there is provided means for preventing the regenerating hot combustion gas from leaking into the stream of the dehydrated air.

30 WHAT WE CLAIM IS:-

1. A dehydration assembly for dehydrating atmospheric air to be supplied to a blast furnace, comprising:

a casing, the inside space of which is 35 divided into regenerating and dehydrating

zones by a partition plate;

at least one gas permeable rotor containing a regenerative moisture absorbent and rotatably mounted in said casing so as to radially extend across cross-sections of said regenerating and dehydrating zones;

a pre-cooler located in said dehydrating zone upstream of said rotor or rotors with respect to the flow of air to be dehydrated in

45 the dehydrating zone in use;

an after-cooler located in said dehydrating zone downstream of said rotor or rotors;

a relative humidity regulator located in said dehydrating zone between said pre-cooler

and said rotor or rotors;

piping means for circulating heat transfer medium through said relative humidity regulator and through said after-cooler so as to effect heat transfer between the two;

an outlet from the dehydrating zone for dehydrated air leaving said after-cooler, and; an inlet for introducing a hot gas into said

regenerating zone.

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A dehydration assembly in accordance 60 with claim 1, wherein the or each said gas permeable rotor comprises a layer containing the regenerative moisture absorbent and a layer containing an adsorbent capable of adsorbing gaseous impurities contained in the 65 air to be dehydrated, said layer containing the

impurity adsorbent being superimposed on said layer containing the moisture absorbent and located upstream of said layer containing the moisture absorbent with respect to the stream of air in the dehydrating zone in use. whereby the air to be dehydrated passes through said layer containing the impurity adsorbent before it passes through said layer

containing the moisture absorbent. A dehydration assembly in accordance

with claim I, wherein a clearance formed between each of two opposed flat surfaces of the or each said rotor and an edge of said partition plate facing said flat surface of the rotor is sealed by a packing element securely fixed on said edge and having two spaced parallel arms extending lengthwise of said edge and contacting the rotor to form a substantially sealed space and wherein for that space formed upstream of the rotor with respect to the stream of hot gas passing through the regenerating zone in use there is provided means for communicating said space with a region downstream of said rotor

in the regenerating zone. 4. A dehydration assembly for dehydrating atmospheric air to be supplied to a blast

furnace, comprising:

a casing, the inside space of which is divided into regenerating and dehydrating

zones by a partition plate:

at least one gas permeable rotor containing a regenerative moisture absorbent and rotatably mounted in said casing so as to radially extend across cross-sections of said regenerat- 100 ing and dehydrating zones;

a pre-cooler located in said dehydrating zone upstream of said rotor or rotors with respect to the flow of air to be dehydrated in

the dehydrating zone in use;

a first after-cooler located in said dehydrating zone downstream of said rotor or rotors;

a second after-cooler located in said dehydrating zone dowstream of said first after-

a relative humidity regulator located in said dehydrating zone between said pre-cooler and said rotor or rotors;

piping means for circulating heat transfer medium through said relative humidity regulator and through said second after-cooler so as to effect heat transfer between the two;

an outlet from the dehydrating zone for the dehydrated air leaving said second aftercooler, and

an inlet for introducing a hot gas into said

regenerating zone.

5. A dehydration assembly in accordance with claim 4, wherein the or each said gas permeable rotor comprises a layer containing 125 the regenerative moisture absorbent and a layer containing an adsorbent capable of adsorbing gaseous impurities contained in the air to be dehydrated, said layer containing the impurity adsorbent being superimposed on 130

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said layer containing the moisture absorbent and located upstream of said layer containing the moisture absorbent with respect to the stream of air in the dehydrating zone in use, whereby the air to be dehydrated passes through said layer containing the impurity adsorbent before it passes through said layer containing the moisture absorbent.

containing the moisture absorbent.

6. A dehydration assembly in accordance with claim 4, wherein a clearance formed between each of two opposed flat surfaces of the or each said rotor and an edge of said partition plate facing said flat surface of the rotor is sealed by a packing element securely fixed on said edge and having two spaced parallel arms extending lengthwise of said edge and contacting the rotor to form a substantially sealed space and wherein for that space formed upstream of the rotor with 20 respect to the stream of hot gas passing through the regenerating zone in use there is provided means for communicating said space with a region downstream of said rotor

in the regenerating zone.

7. A dehydration assembly as described

herein with reference to the accompanying drawings.

8. A blast furnace installation wherein dehydrated air is supplied to the furnace by a blower, and an air dehydration assembly 30 according to any one of the preceding claims is arranged with its outlet from the dehydrating zone connected to the input side of the blower, and its inlet to the regenerating zone connected with a source of combustion gas 35 obtained by burning a waste gas containing inflammable components.

9. A blast furnace installation according to claim 8 wherein said waste gas is a waste gas from the blast furnace.

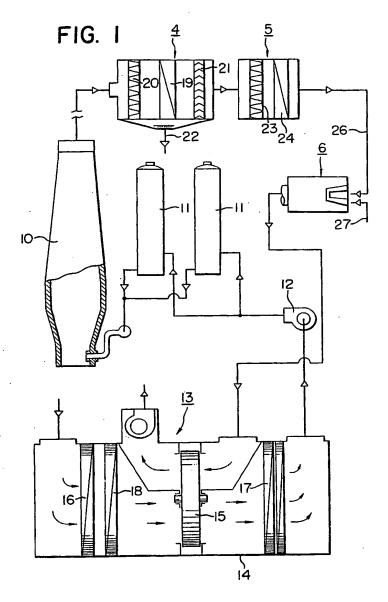
A blast furnace installation as described herein with reference to the accompanying drawings.

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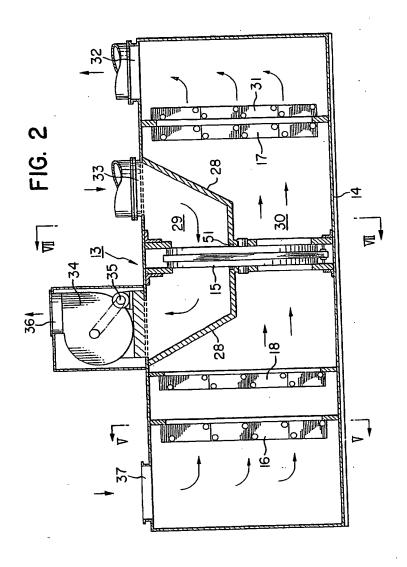
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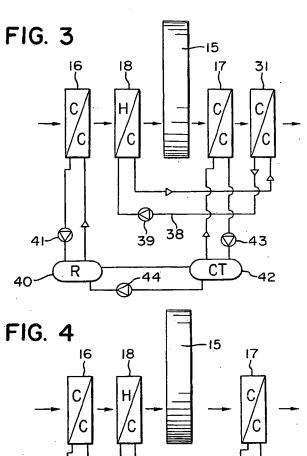


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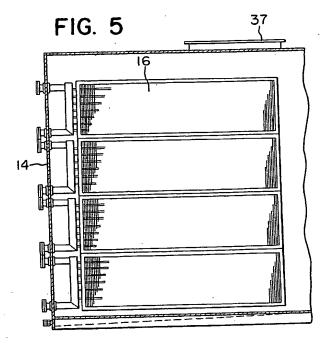


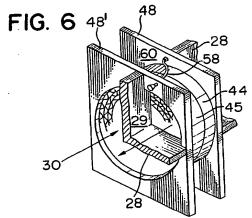
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FIG. 7

